

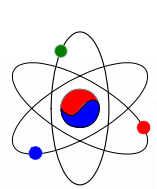
KAERI

Workshop on Advanced Reactors
With Innovative Fuels
ARWIF-2005

MATERIALS PROPERTIES AND FUEL PERFORMANCE OF THE DUPIC FUEL

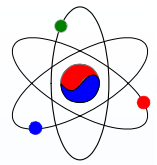
Ho Jin Ryu, Je Sun Moon, Kweon Ho Kang, Kee
Chan Song, and Myung Seung Yang

16-18 Feb. 2005, Oak Ridge, Tennessee



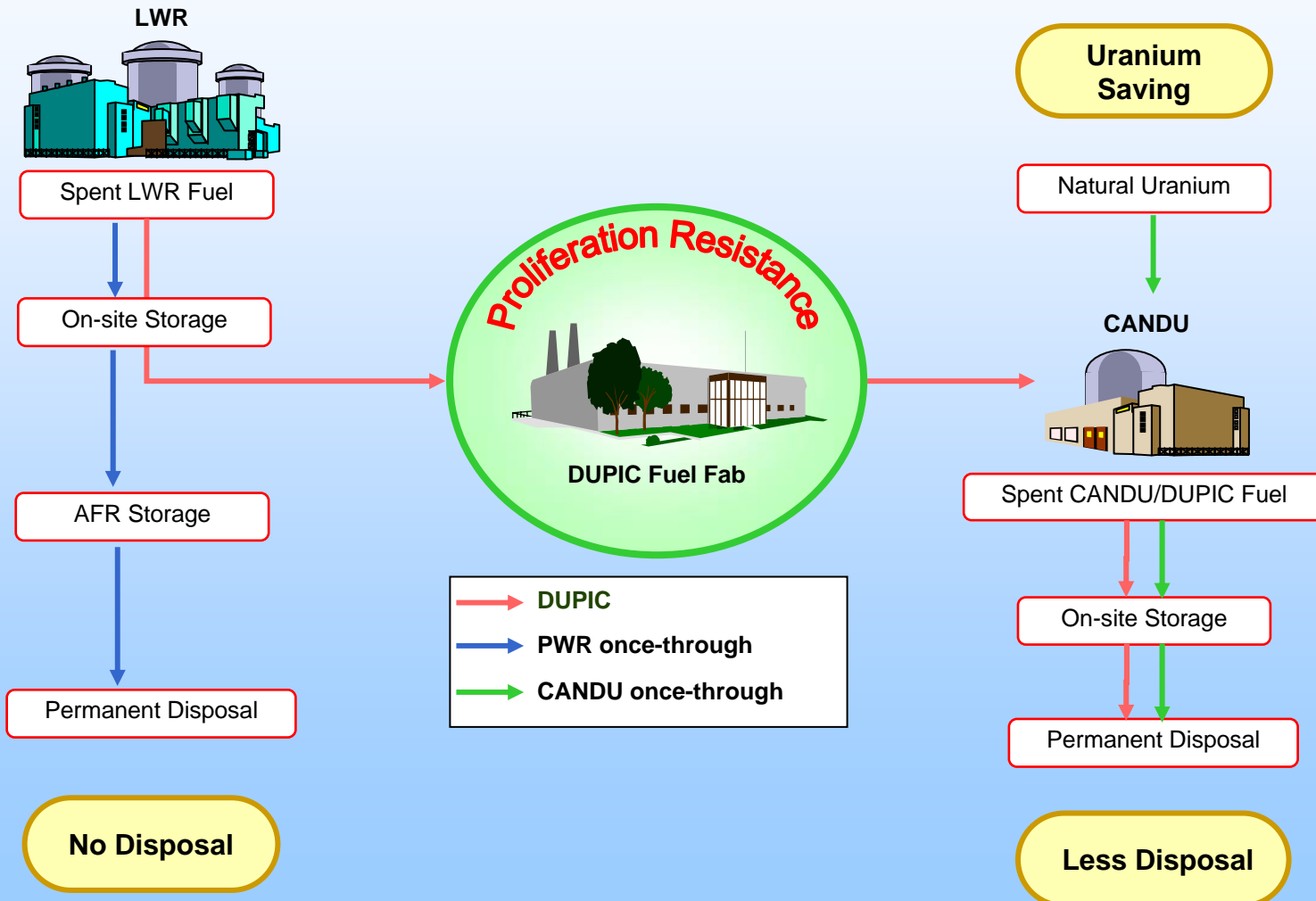
Contents

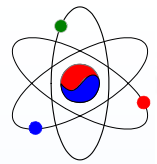
- ◆ **Introduction to the DUPIC Fuel Cycle**
- ◆ **Material Properties of the DUPIC Fuel Pellet**
- ◆ **Performance Analysis of the DUPIC Fuel**
- ◆ **Irradiation Test of the DUPIC Fuel**



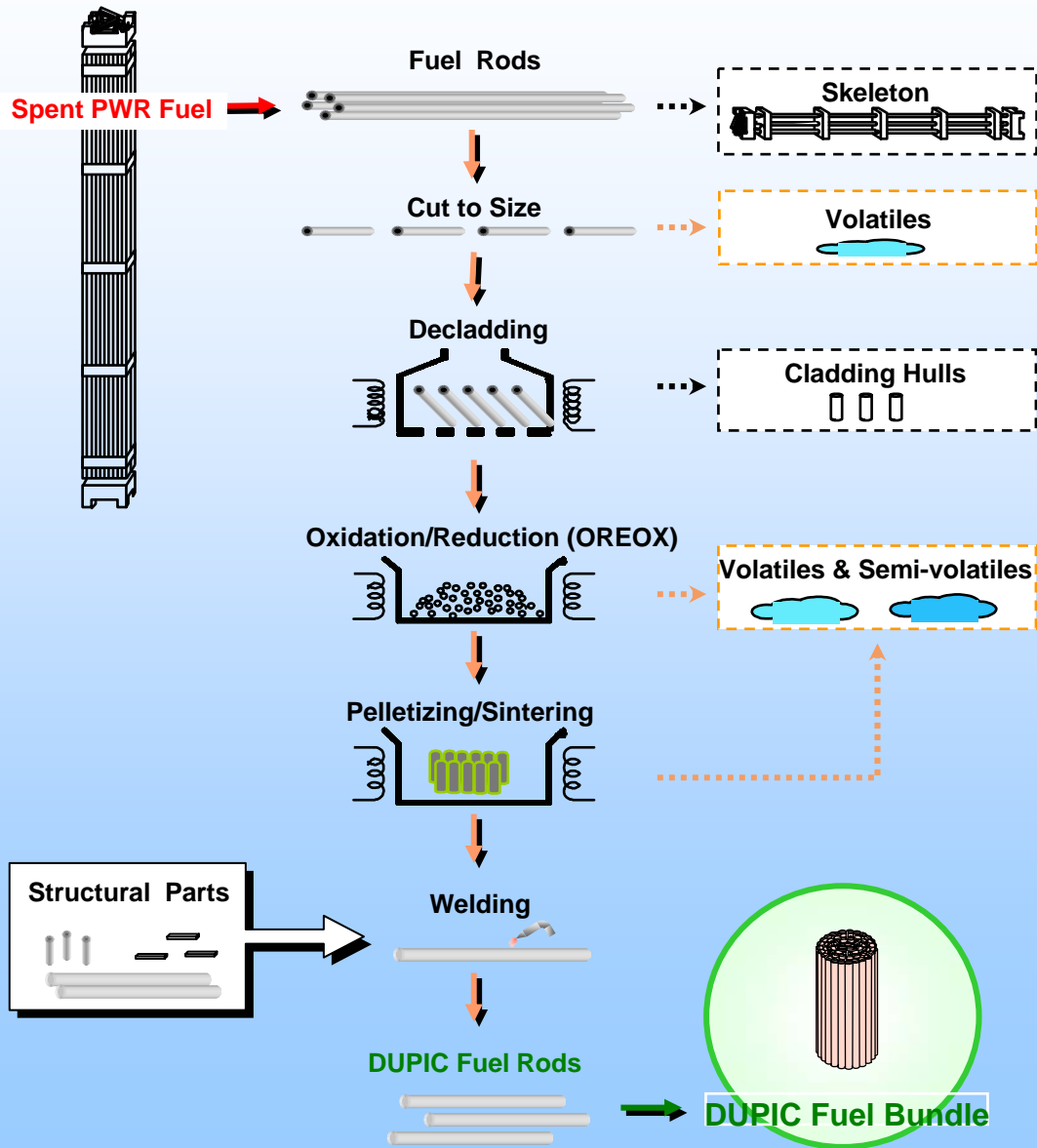
Concept of DUPIC

* **DUPIC** : Direct use of spent PWR fuel in CANDU reactors



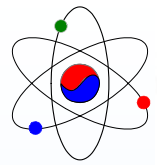


Fabrication Process of DUPIC



Technical Challenges

- Remote fabrication
- Remote handling
- Performance verification of the DUPIC fuel



Material Properties Characterization

➤ Simulated DUPIC fuel

- Due to high radioactivity of spent fuel
- Inactive isotope for fission product elements

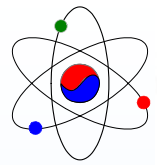
➤ Thermal Properties

- Thermal conductivity
- Thermal expansion coefficient

➤ Mechanical Properties

- Creep rate
- Young's modulus

➤ Diffusion Coefficient of Fission Gas (Xe)



Thermal Properties

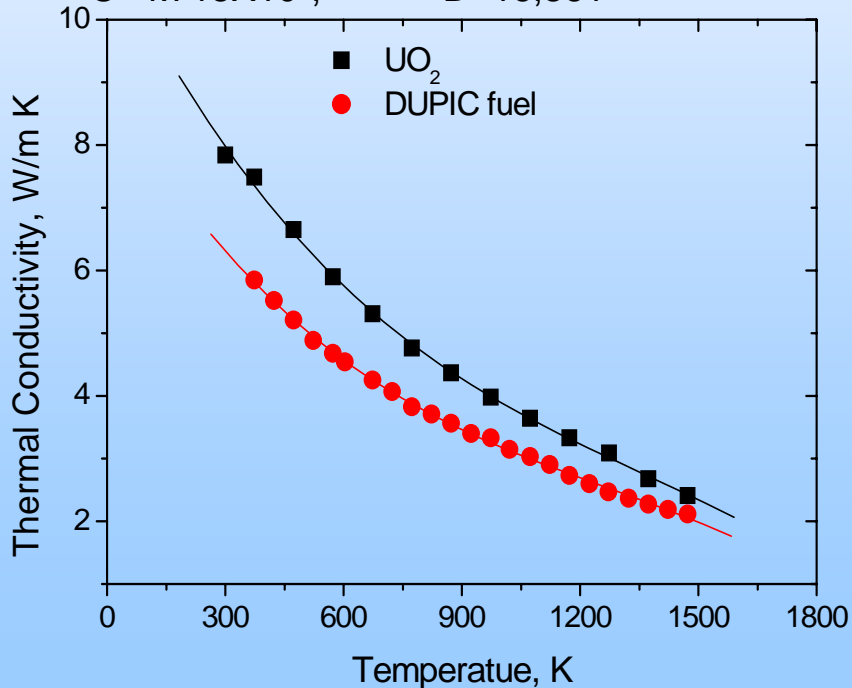
● Thermal Conductivity

Measured by Laser Flash Method

DUPIC < UO₂

$$K_{D0} = \frac{1}{A + BT} + \frac{C}{T^2} \exp\left(-\frac{D}{T}\right)$$

A=0.0944, B=2.027X10⁻⁴,
C=4.715X10⁹, D=16,361

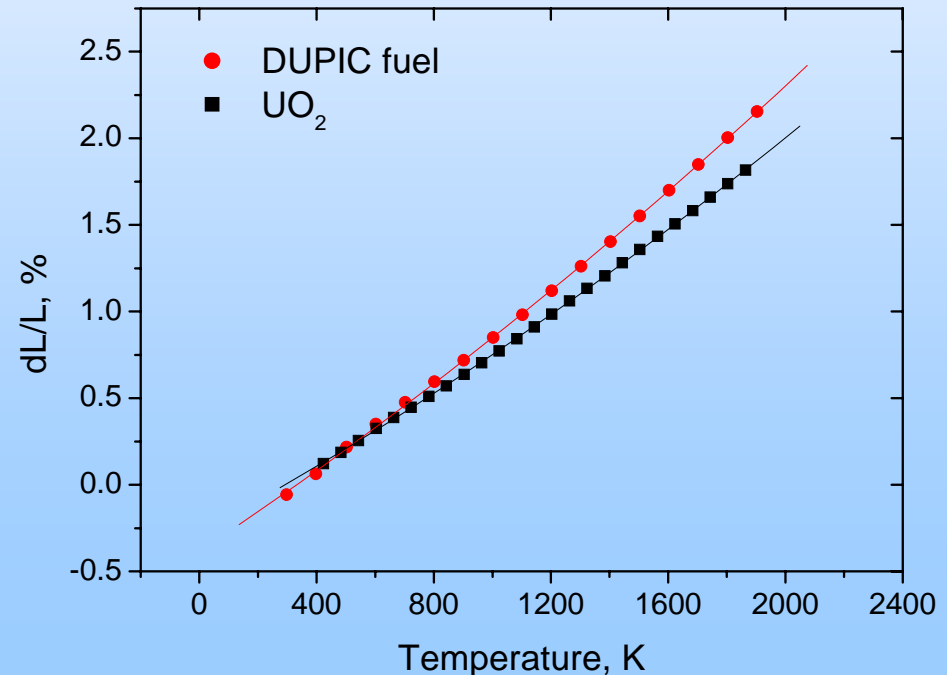


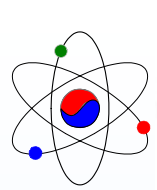
● Thermal Expansion

Measured by Dilatometer (DIL 402C)

DUPIC > UO₂

$$\Delta L / L_0, \% = -0.3854 + 1.130 \times 10^{-3} T + 1.095 \times 10^{-7} T^2$$



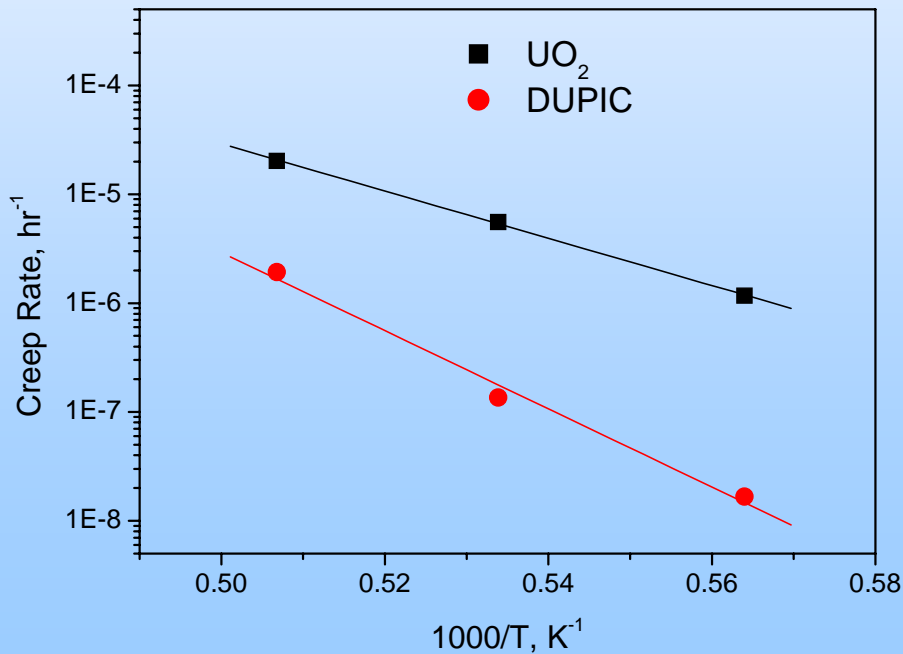


Mechanical Properties

● Creep Rate

Measured by Compressive Creep Test

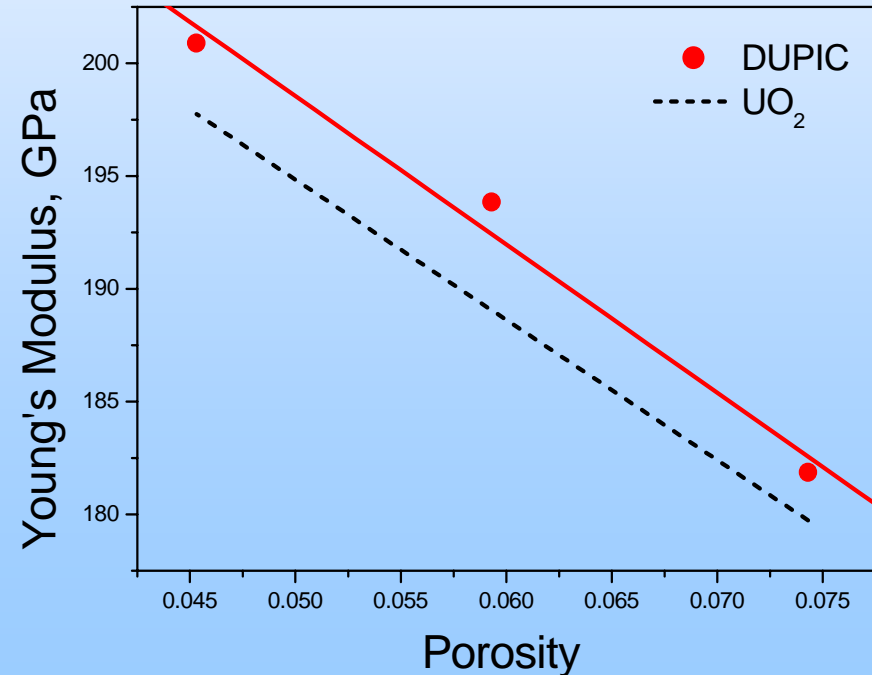
DUPIC < UO₂

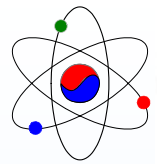


● Young's Modulus

Measured by Resonance Ultrasound Spectroscopy

DUPIC > UO₂

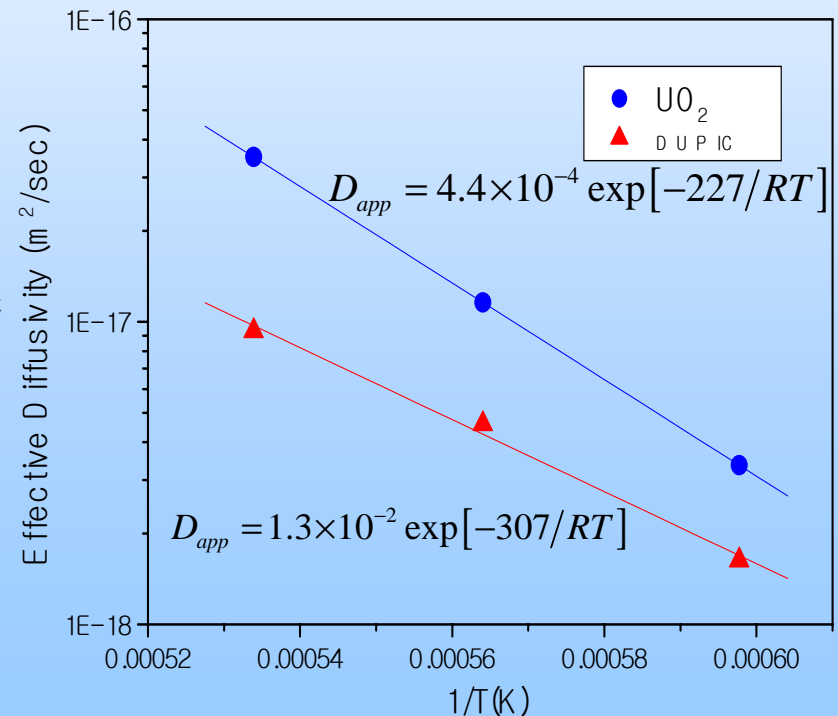
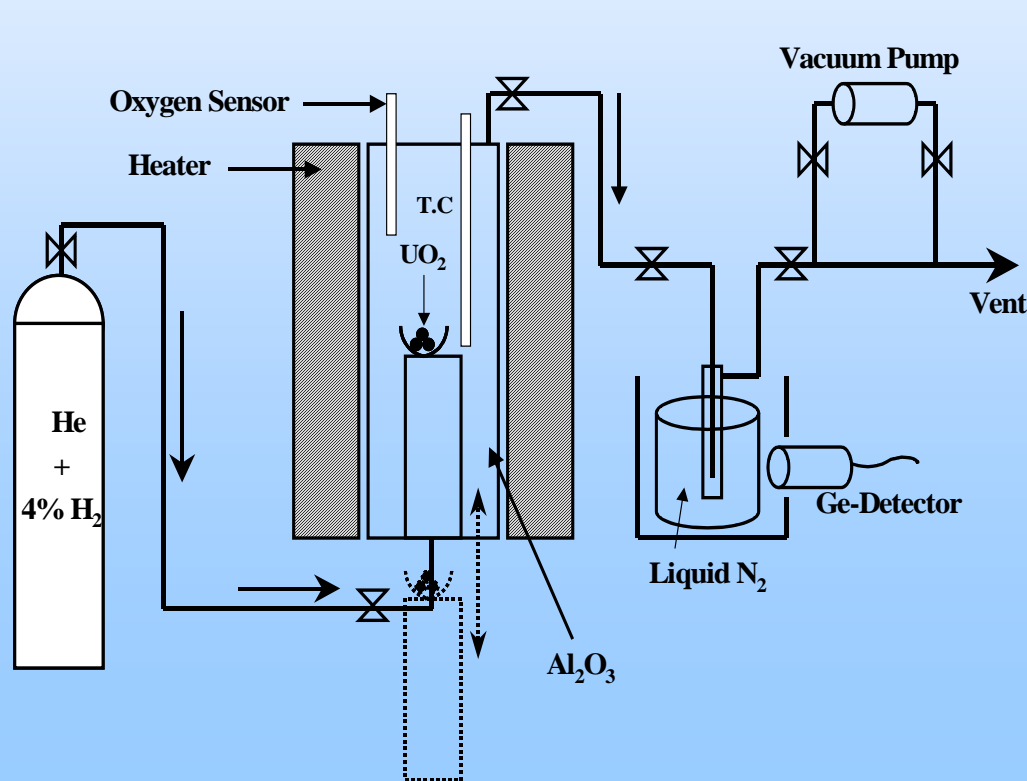


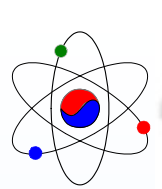


Fission Gas Diffusion Property

Trace Irradiation in the HANARO reactor

- Post-irradiation annealing : 1400 ~ 1600°C
- Diffusion coefficient of Xe-133 : **UO₂ > DUPIC**
- Cation vacancy concentration change by fission products (trivalent)

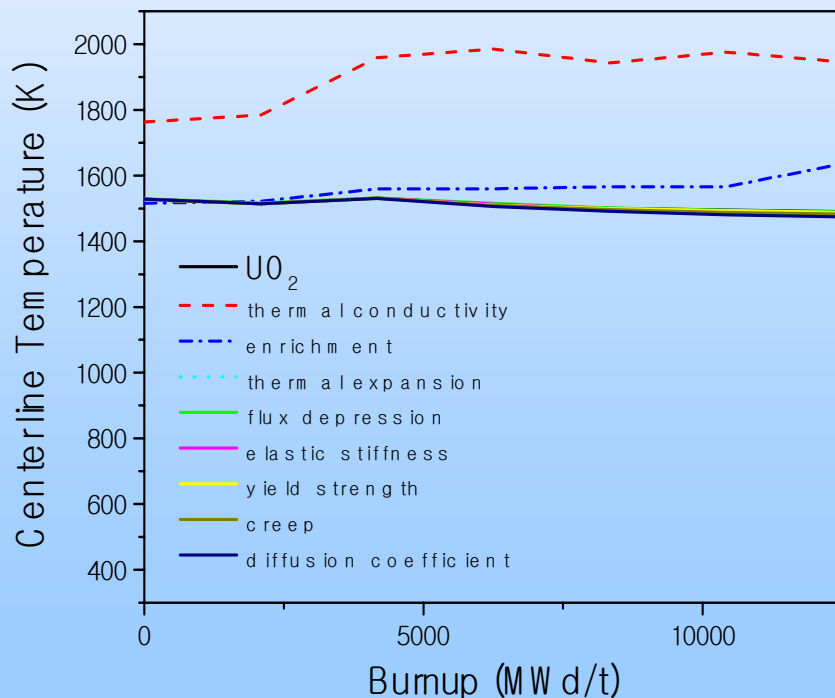




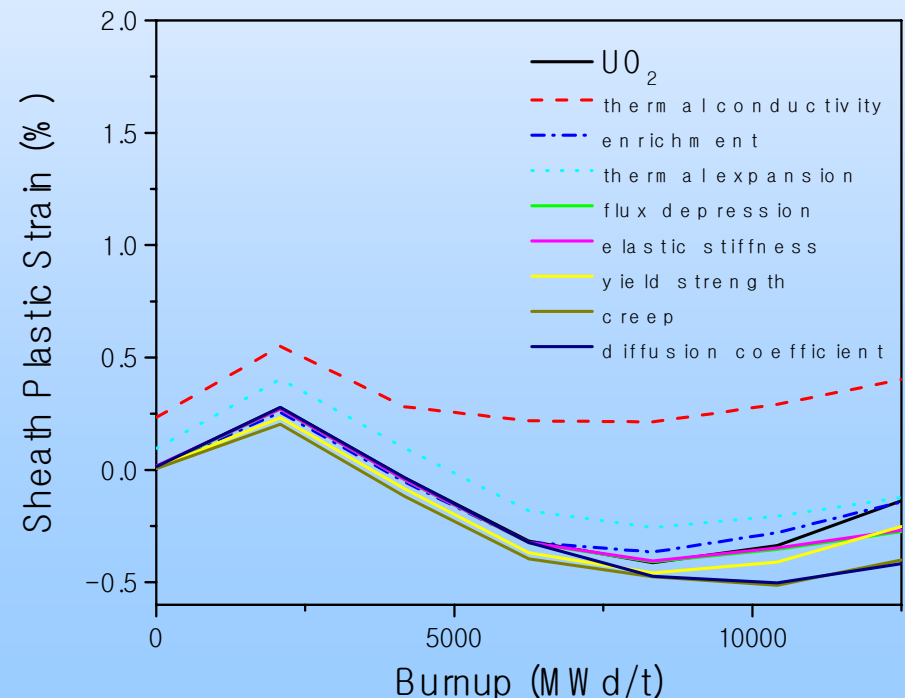
Basic Sensitivity Analysis

- Fuel Performance Code: ELESTRES (AECL)
- Modifying ELESTRES' material models for the DUPIC

Centerline Temperature



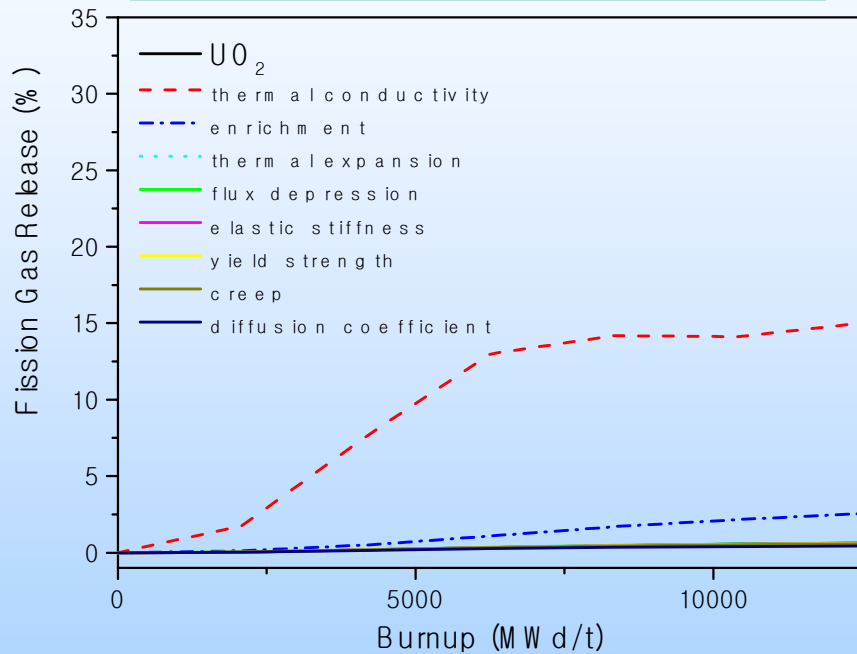
Sheath Plastic Strain



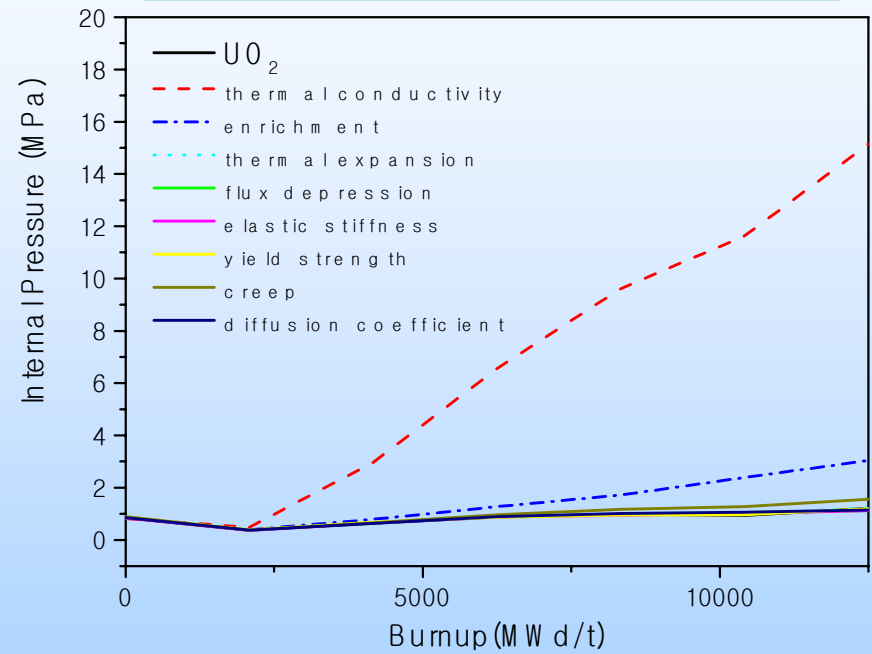


Basic Sensitivity Analysis

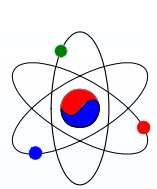
Fission Gas Release



Internal Gas Pressure

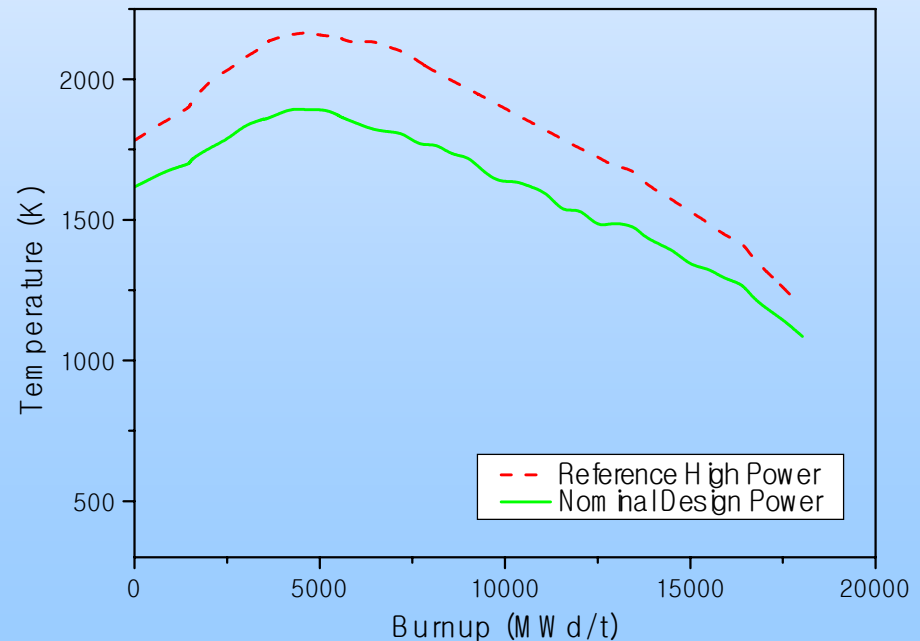
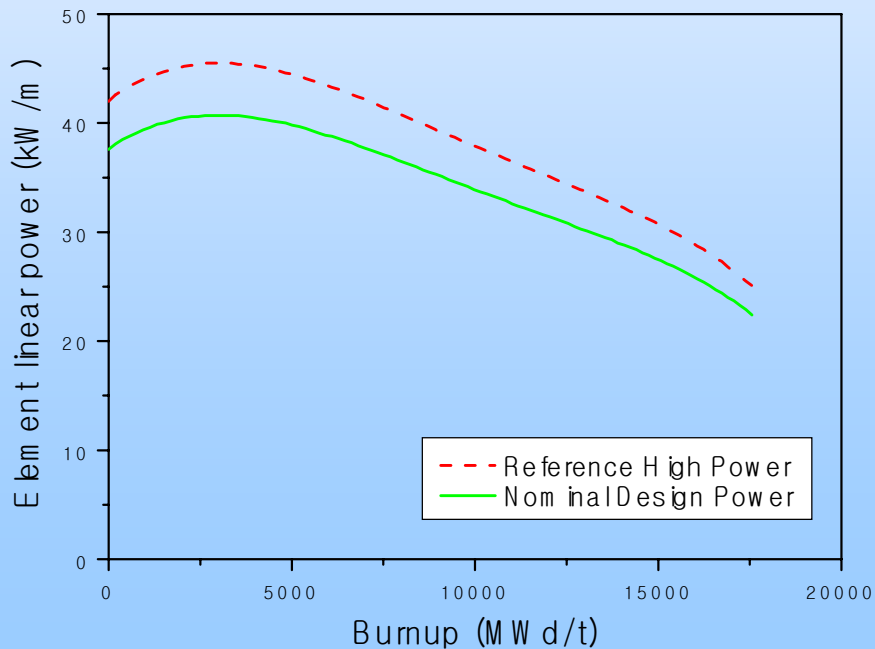


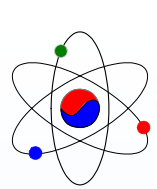
◆ The change of **thermal conductivity** influences most strongly on fuel performance of the DUPIC fuel.



Performance Analysis

- Performance Evaluation by Calculated Power Envelop
 - Reference High Power Envelop
 - Nominal Design Power Envelop
- Higher Temperature than UO_2 but less than melting temp.
 - ~3000 K



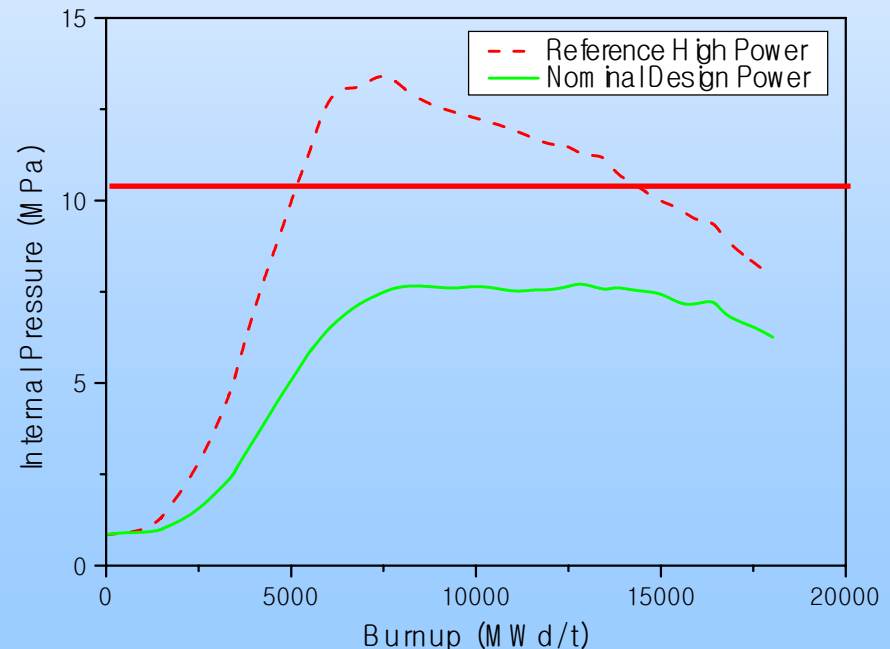
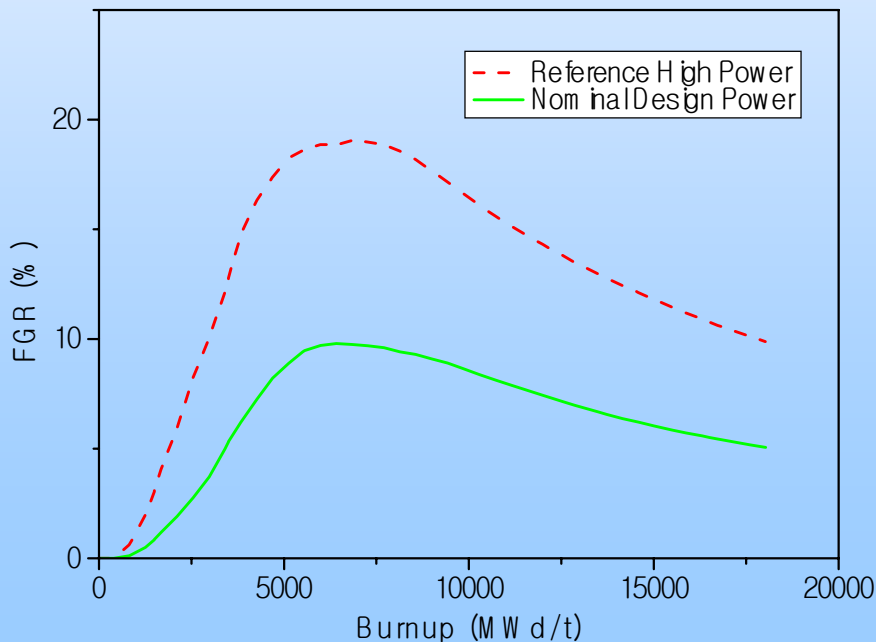


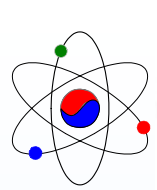
Performance Analysis

Higher fission gas release:

- Due to lower thermal conductivity and resulting higher temperature
- Results in higher internal gas pressure than coolant pressure
- Gap open and outward creep of clad

Internal gas pressure should be reduced.

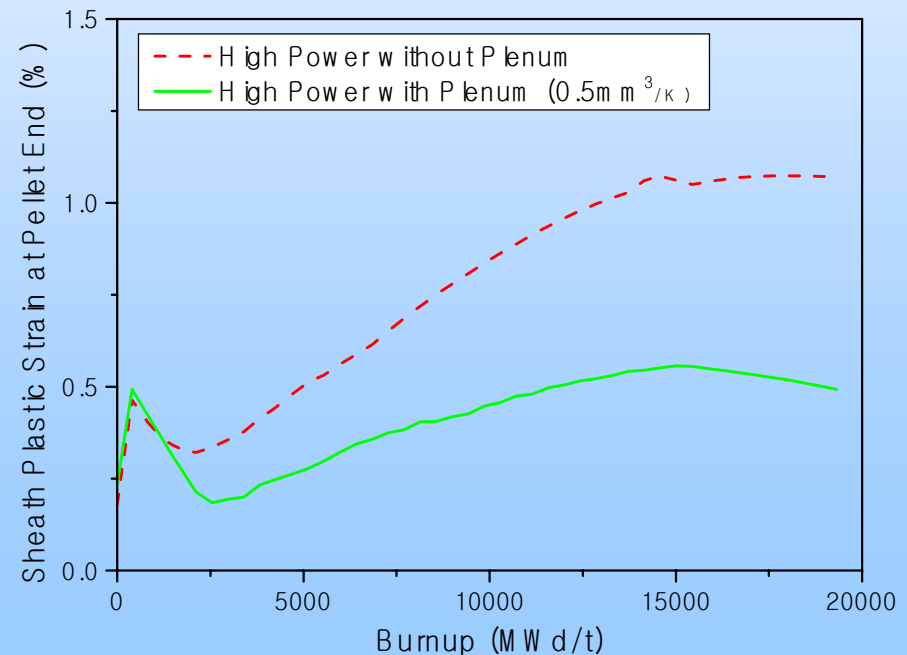
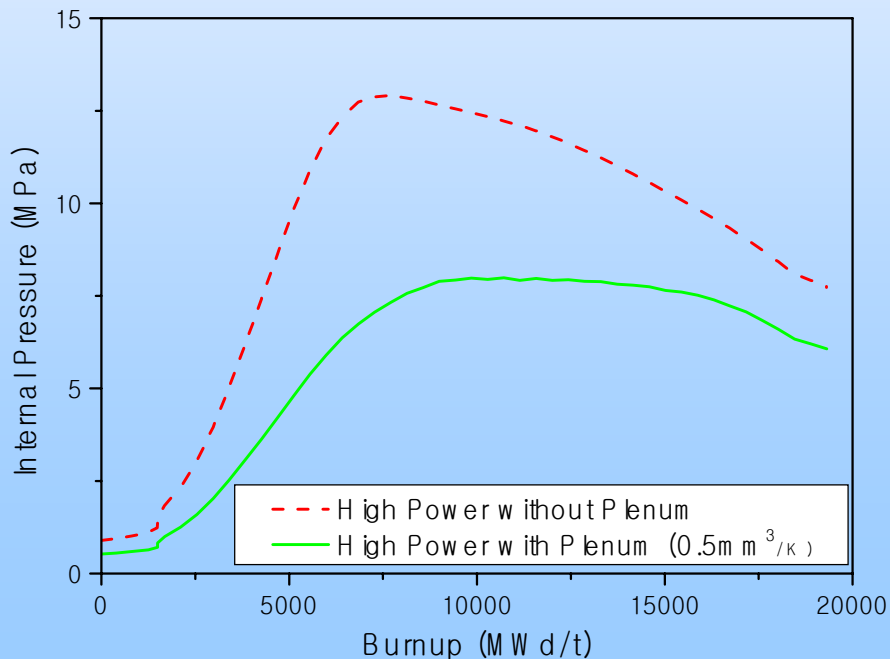


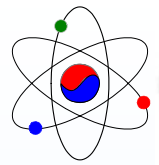


Internal Gas Pressure

➔ One way to reduce the internal gas pressure is to give more volume for fission gases.

- Plenum
- Radial gap
- Axial gap





Orthogonal Array Design

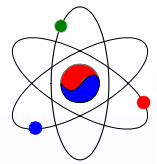
Assignment of the levels to the factors

level	gap clearance (μm)	pellet density (g/cm^3)	grain size (μm)
1	40	10.30	5
2	80	10.45	15
3	120	10.60	25

* within manufacturing spec.

3 level OAD Table, $L_9(3^4)$

Run	factors			
	gap clearance	pellet density	error	grain size
1	1	1	1	1
2	1	2	2	2
3	1	3	3	3
4	2	1	2	3
5	2	2	3	1
6	2	3	1	2
7	3	1	3	2
8	3	2	1	3
9	3	3	2	1

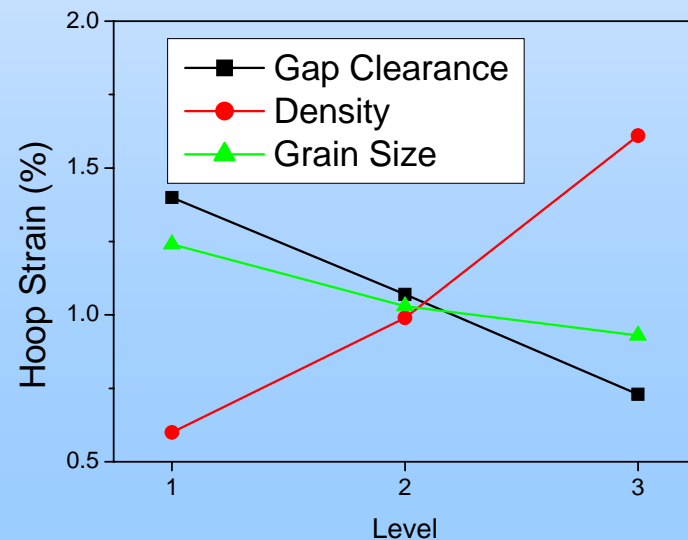
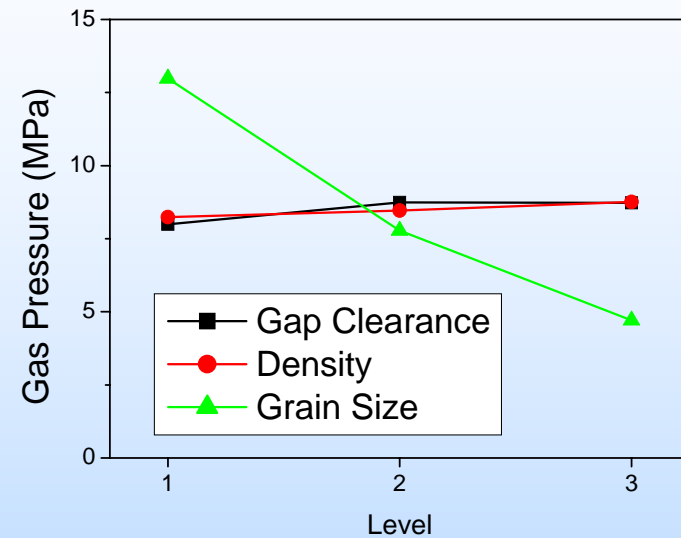
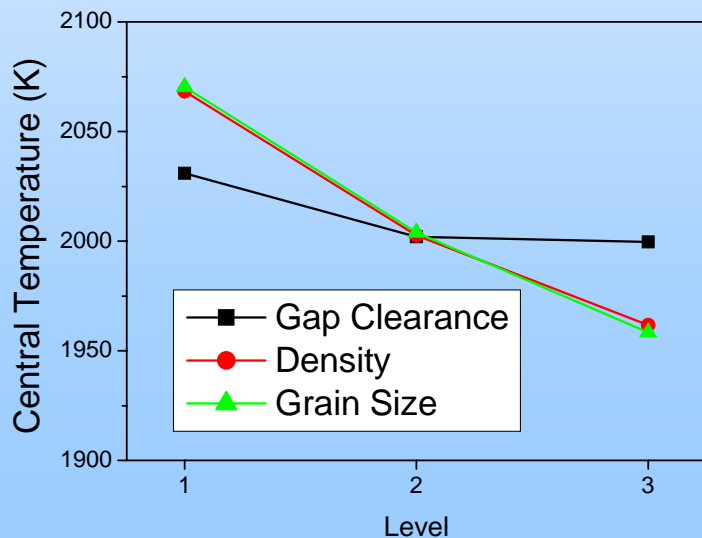


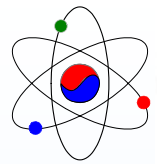
Level-average Response Graphs

➤ Safety Limiting Parameters

- centerline temperature
- Internal gas pressure
- hoop strain

gap & grain \uparrow , density \downarrow





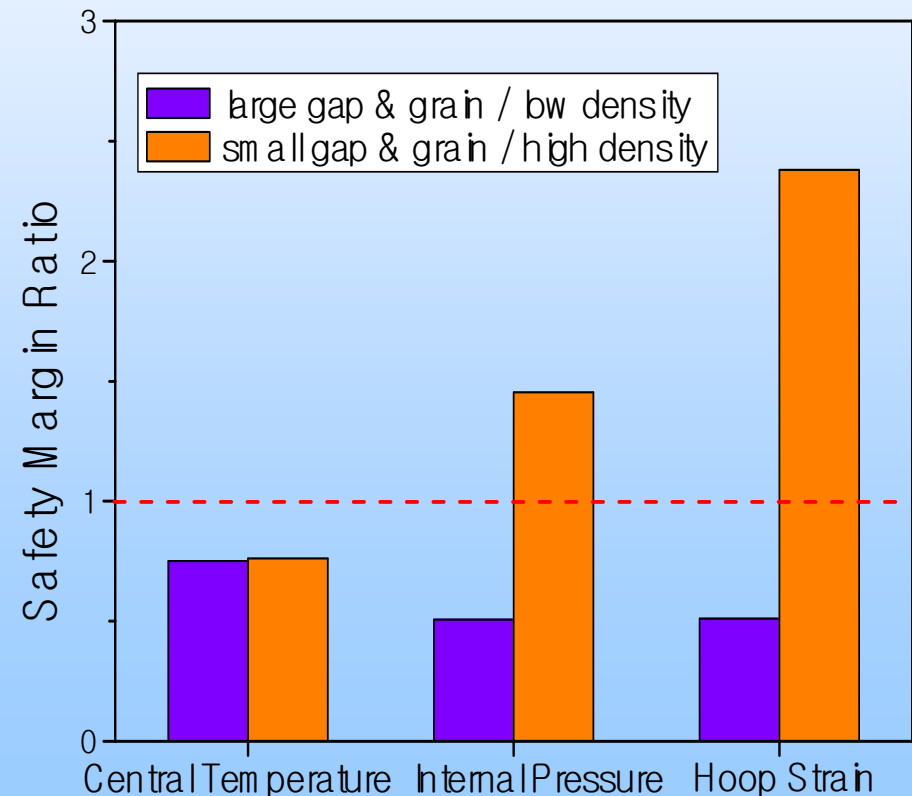
Safety Margin

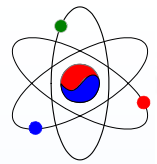
Comparison of Fabrication Factors' Set

- Large gap, large grain, low density
- Small gap, small grain, high density

Safety Margin Standards

- Central temperature: melting temp.
- Internal pressure: coolant pressure
- Hoop strain: 1%

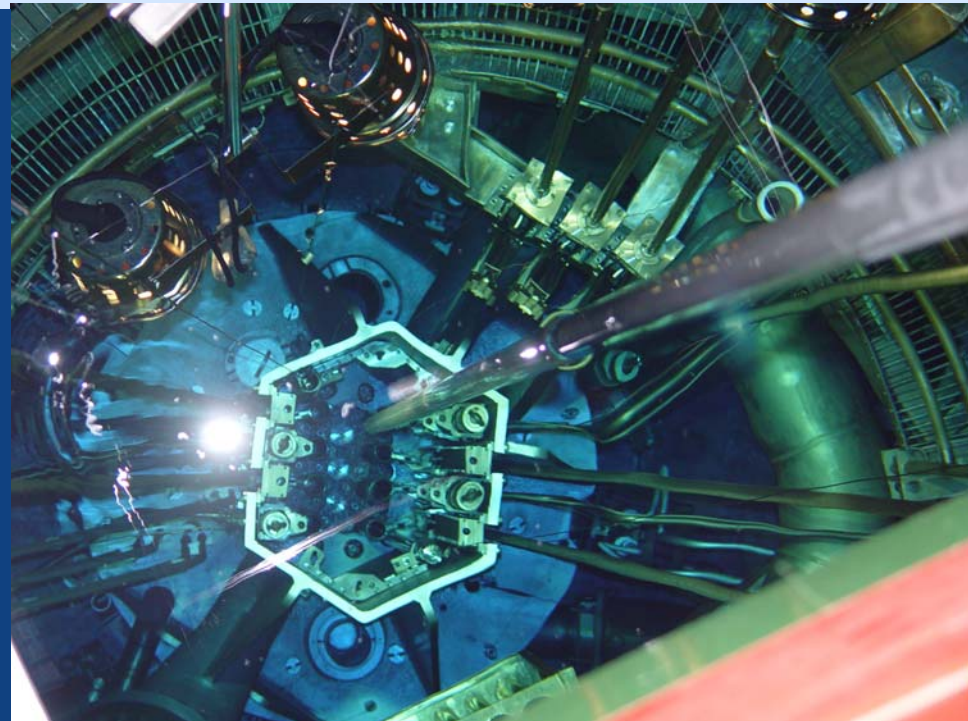


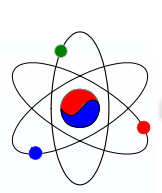


Irradiation Test of DUPIC Fuel

➔ Irradiation Test in HANARO Research Reactor (KAERI)

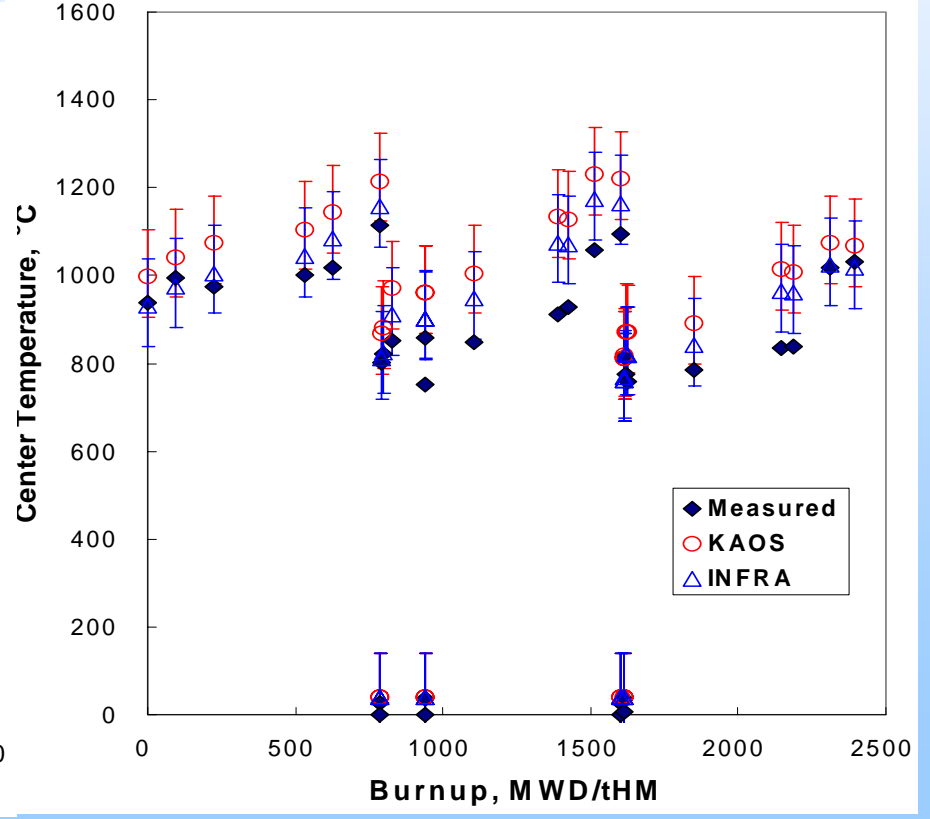
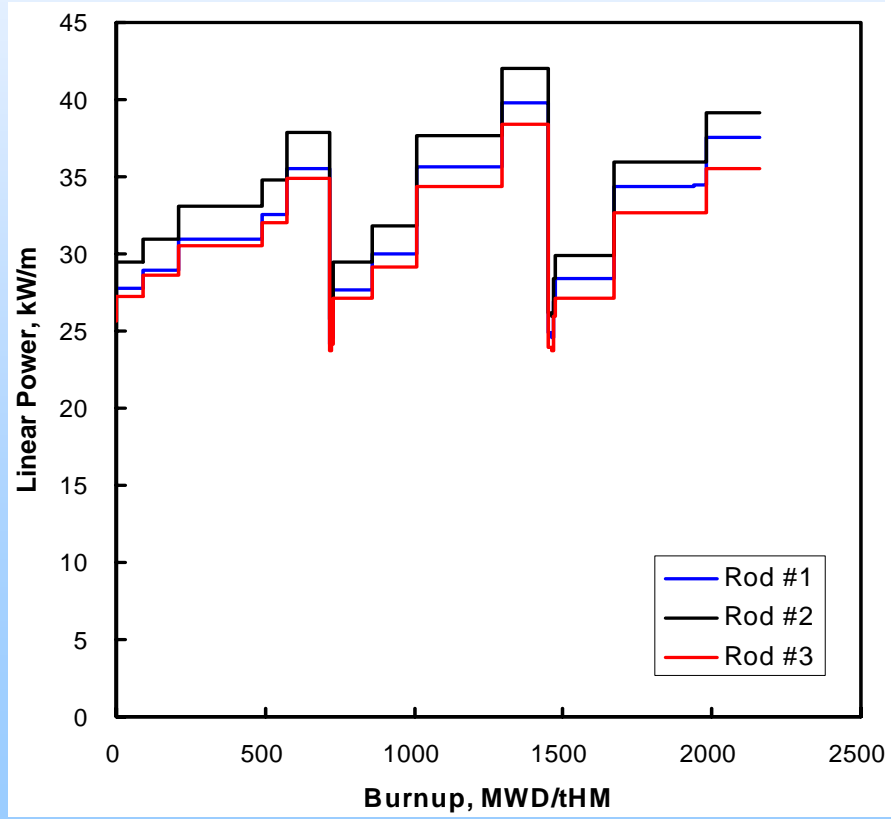
- Spent Fuel: discharged from Gori-1 LWR at 27,300 MWd/tU
- U-235: 1.06%, Pu: 0.51%
- Linear power: ~ 38 kW/m
- Discharge burnup : $\sim 6,700$ MWd/t
- Instrumentation : temp. & SPND

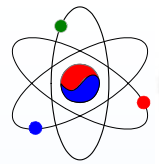




Measured and Calculated Temperature

➤ Good agreement between measured centerline temperature and estimated one calculated by performance evaluation codes

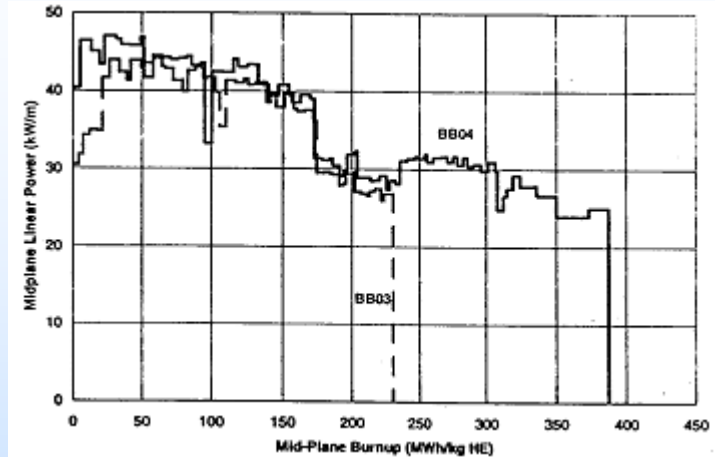




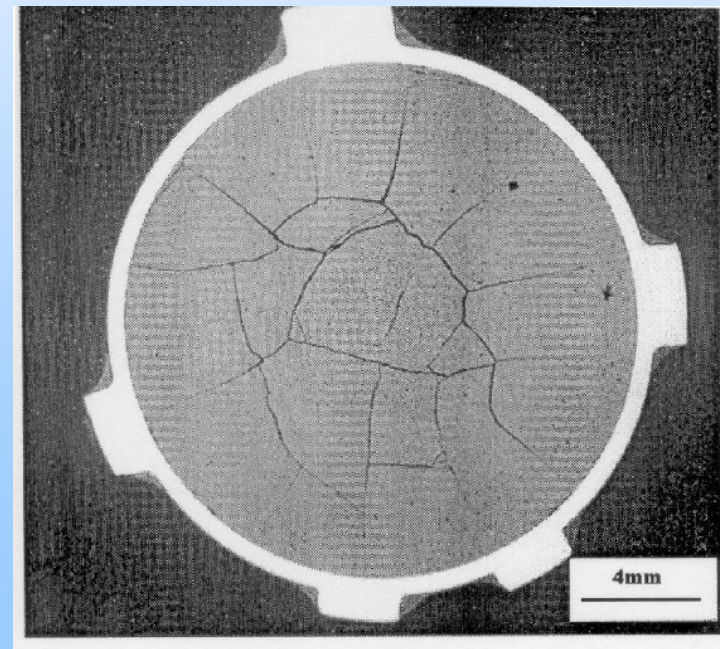
International Collaboration

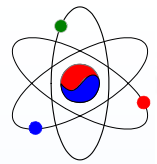
➔ KOREA-CANADA-US-IAEA

- 3 DUPIC Fuel Rod Fabrication (AECL)
- Irradiation Test in the NRU Reactor
- BB03: 2000. Sep. (10 MWd/kgHM)
- BB04: 2001. Dec. (16 MWd/kgHM)
- BB02: 2003. Dec. (21 MWd/kgHM)



Performance Para.	BB03	BB04
Midplane Burnup	10 MWd/kgHM	16 MWd/kgHM
Max. Power	~49 kW/m	~50 kW/m
Max. Ridge Height	0.021 mm	0.029 mm
Residual Sheath Strain (Pellet Interface)	0.2 % to 0.3 %	0.2 % to 0.6 %
Gas Volume	12.6 ml at STP	16.0 ml at STP





Conclusions

- ◆ The material properties of the DUPIC fuel pellet were measured to be used in the fuel performance code for the DUPIC fuel.
- ◆ The fuel performance of the DUPIC fuel shows that the DUPIC fuel requires adjustments of fabrication parameters to guarantee safety margin during the in-reactor operation.
- ◆ The irradiated DUPIC fuel shows good performance in agreement with estimation by performance evaluation codes using material properties for the DUPIC fuel.