

Studsvik

The Metal Recycling Process and its Nuclide Distribution

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Agenda

- Introduction
 - Background
 - Purpose
 - Goal
- Metal recycling process
- Material differences in nuclide distribution
- Results, nuclide distribution in ingots
- Literature comparison
- Conclusion

Background

- Increasing documentation requirements for disposed secondary waste remaining after treatment for free release
- Large conservatism in assigned nuclide vectors for radioactive waste intended for treatment for free release by melting
 - Poor forecasting capabilities
- Dismantling work during decommissioning could be better optimized with
 - Less conservative nuclide vectors
 - Better knowledge of the real outcome from melting
 - More waste could therefore be subject for treatment and free release

Purpose

- Investigate the real nuclide distribution in ingots melted at Studsvik and its secondary waste in order to
 - Obtain a good characterization of the inventory
 - Support the free release process of the ingots
 - Create less conservative and more precise nuclide vectors including the secondary waste
 - Give better guidelines to decommissioning projects and dismantling work

Goal

- Establish an accepted formula for the nuclide distribution during the melting process
- Revise the WAC for the Melting facility to allow for a wider scope of waste to be treated for free release

Introduction – Expected nuclide vectors

- NPP BWR and PWR primary circuit standard operation without significant fuel failures
 - Dominant contaminants activation products are Co-60, Ni-63 and Fe-55
- NPP with fuel failure history
 - Also fission products such as Cs-137, Sr-90, and certain alpha emitting nuclides have to be considered as a significant part of the nuclide inventory
- Fuel factories
 - Uranium isotopes and its progeny
 - TRU-elements and activation products (mainly for MOX plants)
- Research facilities (LWR, HWR, Spallation sources)
 - A wide combination of nuclides can exist

Metal recycling process

- Melting is suitable for low level waste with all types of contaminations
 - Both short lived and long lived nuclides can be treated
 - Nuclides in vapor phase at room temperature lead to special requirements for the off-gas treatment
- Established techniques and facilities available
- International recommendation exists
 - EC RP89
- Melting facility at Studsvik since 1987
 - Licensed capacity 5 k tonne per y
 - Induction furnaces



Carbon and stainless steel

- Co, Mn, Fe, Ag and Ni isotopes are closely linked to the steel matrix and stays therefore to a high degree
- Heavy alpha isotopes (U, Am, Pu) will end up in the slag to a high degree
- Nuclides which evaporates at the actual temperature are transferred to the slag or the dust (Cs etc.)

Aluminium

- Co stays in the metal
- Heavy alpha isotopes (U, Am, Pu) stays in the metal to a high degree
- Nuclides which evaporates at the actual temperature are transferred to the slag or the dust

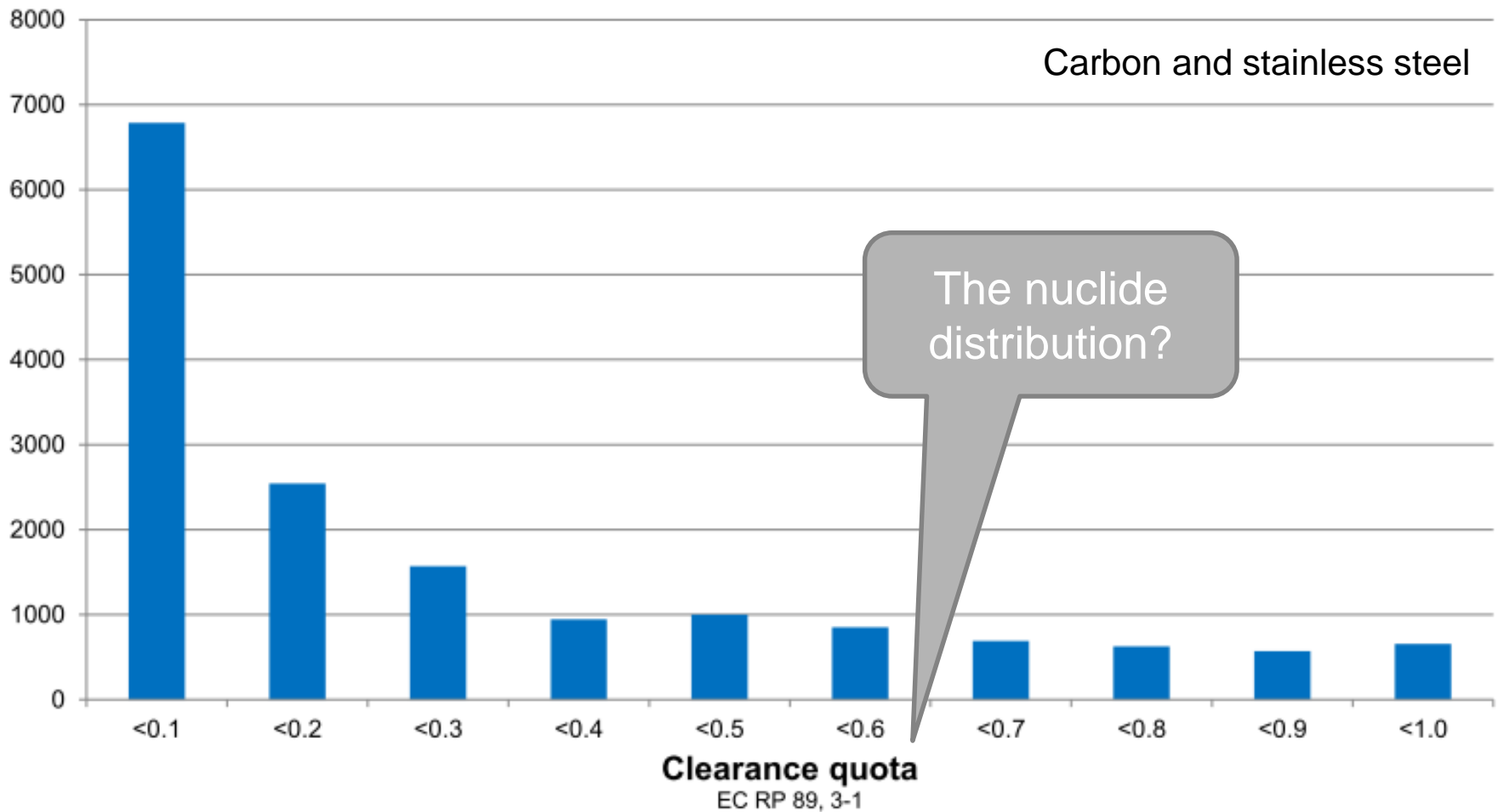
Lead

- Most isotopes can be removed from the metal
- Co end up in the slag
- Certain nuclides such as Ag-108m are hard to separate in the melting process
- Heavy alpha isotopes (U, Am, Pu) ends up in the slag to a high degree
- Nuclides which evaporates at the actual temperature are transferred to the slag or the dust
- Special personnel safety case when handling lead melting!

Overview– most important nuclides [1]

| Nuclide | Mode (α β γ) | T ^{1/2} | Steel (%) | Slag (%) | Dust (%) | Other (%) |
|---------|------------------------------------|------------------|-----------|----------|----------|---------------|
| H-3 | β | 12.33 y | | | | |
| C-14 | β | 5730 y | 27-100 | 0-1 | 0-2 | 0-73 (offgas) |
| Mn-54 | $\beta + \gamma$ | 312 d | 24-100 | 1-75 | 0-5 | 0 |
| Co-60 | $\beta + \gamma$ | 5.27 y | 20-100 | 0-1 | 0-80 | 0 |
| Zn-65 | $\beta + \gamma$ | 244 d | 0-20 | 0-1 | 80-100 | 0 |
| Sr-90 | β | 28.79 y | 0-20 | 95-100 | 0-10 | 0 |
| Ag-108m | $\beta + \gamma$ | 418 y | 75-100 | 0-1 | 0-25 | 1 (bottom) |
| Ag-110m | $\beta + \gamma$ | 249 d | | | | |
| Sb-125 | $\beta + \gamma$ | 2.76 y | 60-100 | 0-20 | 10-40 | 0 |
| Cs-137 | $\beta + \gamma$ | 30.07 y | 0 | 0-5 | 95-100 | 0 |
| U-234 | α | 2.4E+5 y | 0-1 | 95-100 | 0-5 | 0 |
| U-235 | $\alpha + \gamma$ | 7.0E+8 y | | | | |
| U-238 | $\alpha (+ \gamma)$ | 4.5E+9 y | | | | |
| Pu-238 | α | 87.7 y | 0-1 | 95-100 | 0-5 | 0 |
| Pu-239 | α | 24 110 y | | | | |
| Am-241 | $\alpha + \gamma$ | 432 y | 0-1 | 95-100 | 0-5 | 0 |

Histogram over conditionally cleared ingots 2005-2012. Approx. 10 000 tonne



Results, nuclide distribution in ingots

| Material category | Weight, tonne | Measured nuclide content, % of total activity* | | | | | | | | |
|-------------------|---------------|--|-------|--------|--------|-------|---------|--------|-------------|--------|
| | | Co-60 | Mn-54 | Sb-125 | Cs-137 | Zn-65 | Ag-110m | Ru-106 | Total alpha | Others |
| CS and SS | 27 749 | 96% | 1.1% | 0.7% | 0.7% | 0.5% | 0.3% | 0.3% | 0.3% | 0.5% |
| | | | | | (MDA) | | | | | |
| Aluminium | 772 | 62% | 11% | 6.4% | 5.6% | 4.6% | 4.2% | 1.4% | 1.1% | 2.8% |
| | | | | | | | | | | |
| Lead | 395 | 52% | 17% | 5.8% | 5.5% | 5.0% | 3.9% | 3.1% | 1.3% | 6.3% |

*) MDA values included from gamma / alpha spectrometry.

Material differences, melting results

- Carbon and stainless steel
 - Total amount melted 27 700 tonne
 - Includes ingots for direct free release and under decay storage
 - Nuclide distribution in ingots
 - Co-60 >95% of all activity
 - Since Co-60 is totally dominant nuclide and Cs-137 is important to measure, it was decided to concentrate the detailed study on Co-60 and Cs-137
 - 5 200 tonne included for the relation of nuclides in ingots / slag / dust

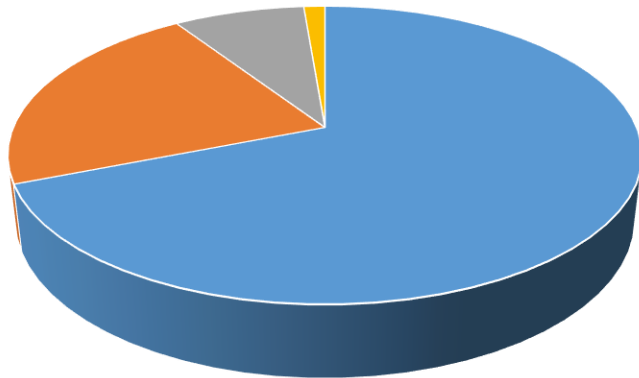
Material differences, metals recycling

- Carbon and stainless steel
 - 5 200 tonne from different LWRs
 - Median levels adds up to 100% reasonably well

| Co-60. | | | | | Cs-137 | | | | |
|-------------------------|--------|-----|-----|--------|-------------------------|--------|-----|-----|--------|
| <u>Container scrap</u> | | Max | Min | Median | <u>Container scrap</u> | | Max | Min | Median |
| Blasting residues | | 91% | 18% | 69% | Blasting residues | | 16% | 1% | 14% |
| Melting fraction | Ingots | 92% | 29% | 67% | Melting fraction | Ingots | 0% | 0% | 0% |
| | Dust | 58% | 6% | 24% | | Dust | 70% | 23% | 57% |
| | Slag | 14% | 2% | 4% | | Slag | 77% | 30% | 52% |
| <u>Large components</u> | | Max | Min | Median | <u>Large components</u> | | Max | Min | Median |
| Pre melting fraction | | 82% | 14% | 46% | Pre melting fraction | | 35% | 10% | 20% |
| Melting fraction | Ingots | 99% | 88% | 97% | Melting fraction | Ingots | 0% | 0% | 0% |
| | Dust | 7% | 0% | 2% | | Dust | 29% | 10% | 15% |
| | Slag | 6% | 1% | 2% | | Slag | 90% | 71% | 85% |

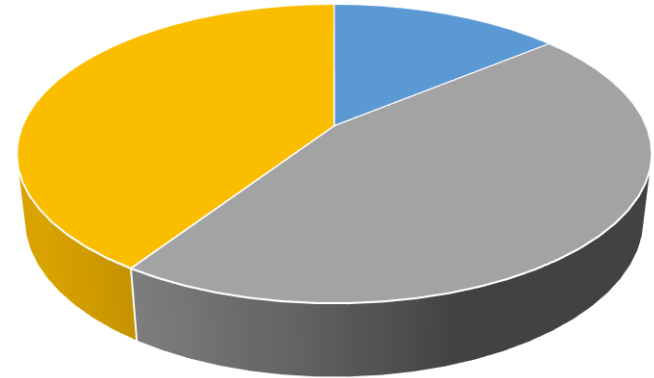
CS and SS, 5200 tonne LWRs, cont.

Co-60, container scrap



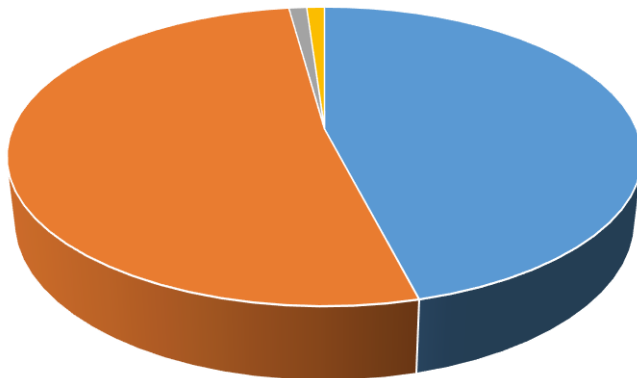
■ Blasting residues ■ Ingots ■ Dust (melting) ■ Slag (melting)

Cs-137, container scrap



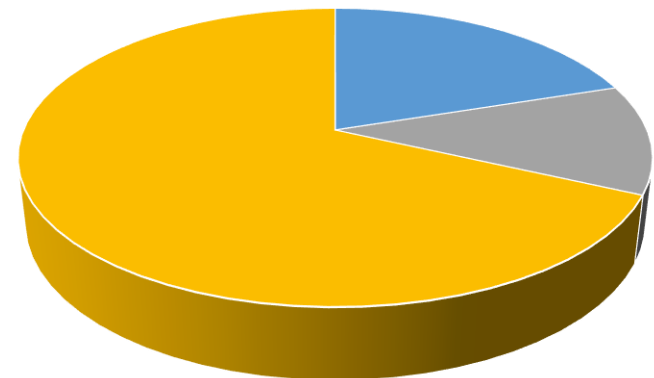
■ Blasting residues ■ Ingots ■ Dust (melting) ■ Slag (melting)

Co-60, large components



■ Pre melting ■ Ingots ■ Dust (melting) ■ Slag (melting)

Cs-137, large components



■ Pre melting ■ Ingots ■ Dust (melting) ■ Slag (melting)

CS and SS, 5200 tonne LWRs, cont.

For the metal recycling process

- Co-60
 - Melting in combination with blasting and pre melting actions is effective.
- Cs-137
 - Melting is the outstanding most effective individual step, and can be used in combination with blasting and pre melting actions

Material differences, metals recycling

- Al
 - Total amount melted 800 tonne
 - Nuclide distribution
 - Co-60 dominating with >60%
 - Top six corresponds to 95%

Material differences, metals recycling

- Lead
 - Total amount melted 400 tonne
 - All ingots free released
 - Nuclide distribution
 - Sr-90 dominating with >50%
 - Top six corresponds to 89%
 - More ingots needed to sort out normal vs. unusual cases

Literature comparison

1. NCRP (2002). Managing Potentially Radioactive Scrap Metal, NCRP Report No 141, NCRP, Bethesda, MD.
 - Table 6.2, Applicable for steel
 - Large uncertainty for some nuclides (combined information from different sources)
2. QUADE, U. and MÜLLER, W. (2005). Recycling of radioactively contaminated scrap from the nuclear cycle and spin-off for other application, Rev. Metal. Madrid Vol. Extr. (2005) 23-28.
 - Table 1, Applicable for steel
 - Detailed nuclide distribution for many nuclides

Literature comparison, CS and SS

| Nuclide | Ref. | Note | Steel (%) | Slag(%) | Dust (%) | Other (%) |
|---------|-----------|-----------|-----------|---------|----------|-----------|
| Co-60 | [1] | | 20-100 | 0-1 | 0-80 | 0 |
| | [2] | | 88 | 11 | 1 | 0 |
| | Container | Min - Max | 29-92 | 2-14 | 6-58 | 0 |
| | Container | Median* | 70 | 4 | 26 | 0 |
| | LC | Min - Max | 88-99 | 1-6 | 0-7 | 0 |
| | LC | Median* | 96 | 2 | 2 | 0 |
| Cs-137 | [1] | | 0 | 0-5 | 95-100 | 0 |
| | [2] | | <1 | 60 | 40 | 0 |
| | Container | Min - Max | 0-0 | 30-77 | 23-70 | 0 |
| | Container | Median* | 0 | 47 | 53 | 0 |
| | LC | Min - Max | 0-0 | 71-90 | 10-29 | 0 |
| | LC | Median* | 0 | 85 | 15 | 0 |

*) Median value re-scaled to 100% total sum

Conclusions

- Carbon and stainless steel
 - Co-60
 - Totally dominating measured nuclide in the ingots (>95%)
 - Confirmed literature data regarding relationship between ingots, slag, and, dust
- Aluminium
 - Co-60 dominating with >60%
- Lead
 - All ingots free released

Conclusions, cont.

- Investigated the real nuclide distribution in ingots melted at Studsvik and its secondary waste
 - Obtained a good characterization of the inventory
 - Supported the free release process of the ingots
 - Created less conservative and more precise nuclide vectors including the secondary waste
 - Able to give better guidelines to decommissioning projects and dismantling work
- Important step in order to develop improved models for the nuclide distribution during the melting process
- Supporting both waste generators and disposal organizations in their optimization work

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